



## Design study of a 10 MW MgB<sub>2</sub> superconductor direct drive wind turbine generator

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## Abstract

A design study of a 10 MW direct drive wind turbine generator based on MgB<sub>2</sub> superconducting wires is presented and the cost of the active materials of the generator is estimated to be between 226 €/kW and 84 €/kW, which is lower than the threshold values of 300 €/kW of the INNWIND.EU project. A nacelle structure with a front-mounted generator is presented for further investigation of the integration of such a superconducting generator into offshore turbines with power ratings considerably larger than 10 MW.

## Nacelle and Generator

### Motivation:

The INNWIND.EU project is investigating the feasibility of superconducting direct drive generators for offshore turbines ranging up to 20 MW [1]. A king-pin nacelle design is proposed as template for comparing different generators in terms of cost and cost of energy. Features of the drive train are outlined below:

### Nacelle

- Static King-Pin and two main bearings supporting hub
- $P = 10$  MW,  $T = 10.6$  MNm @ 9.65 rpm

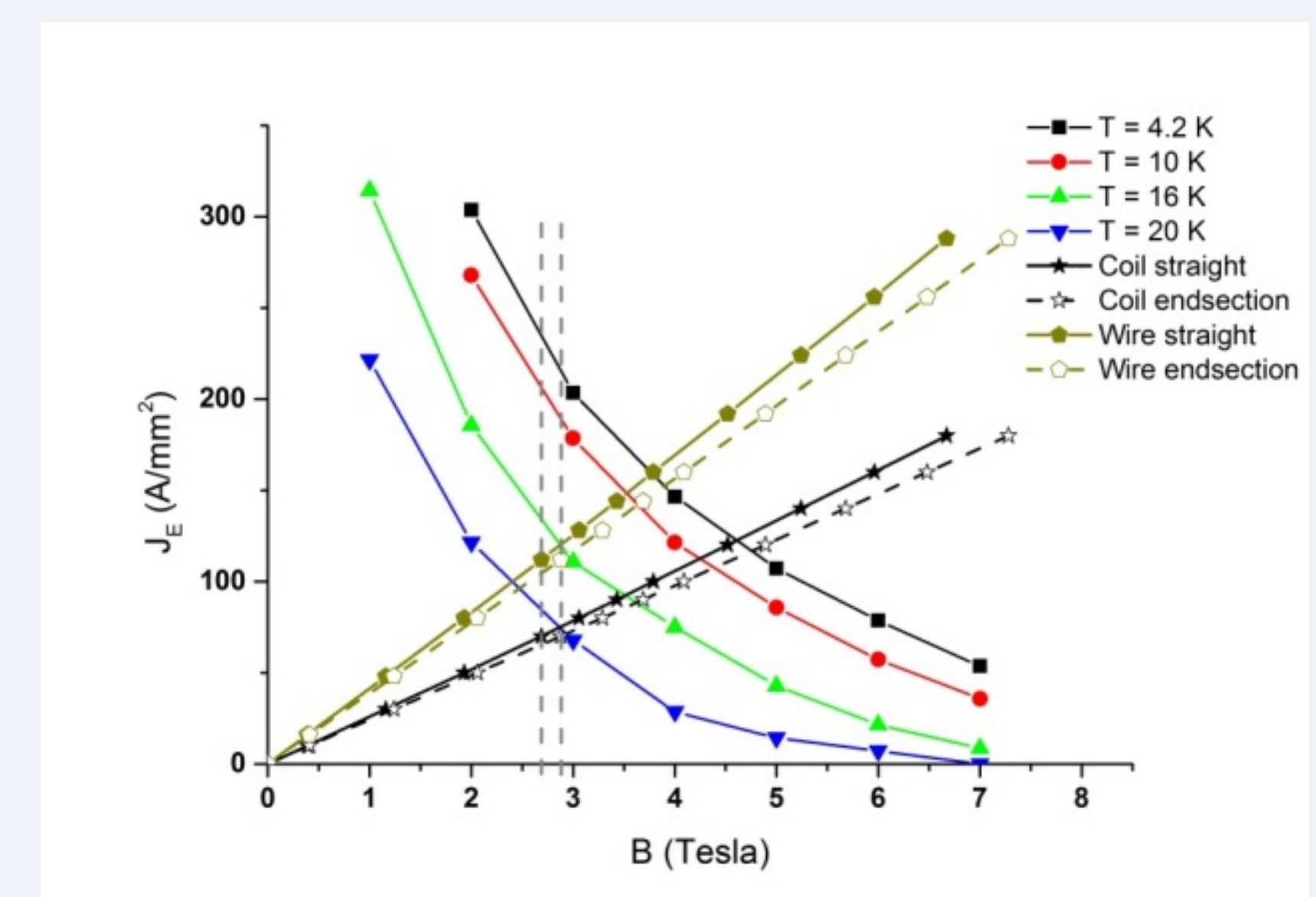
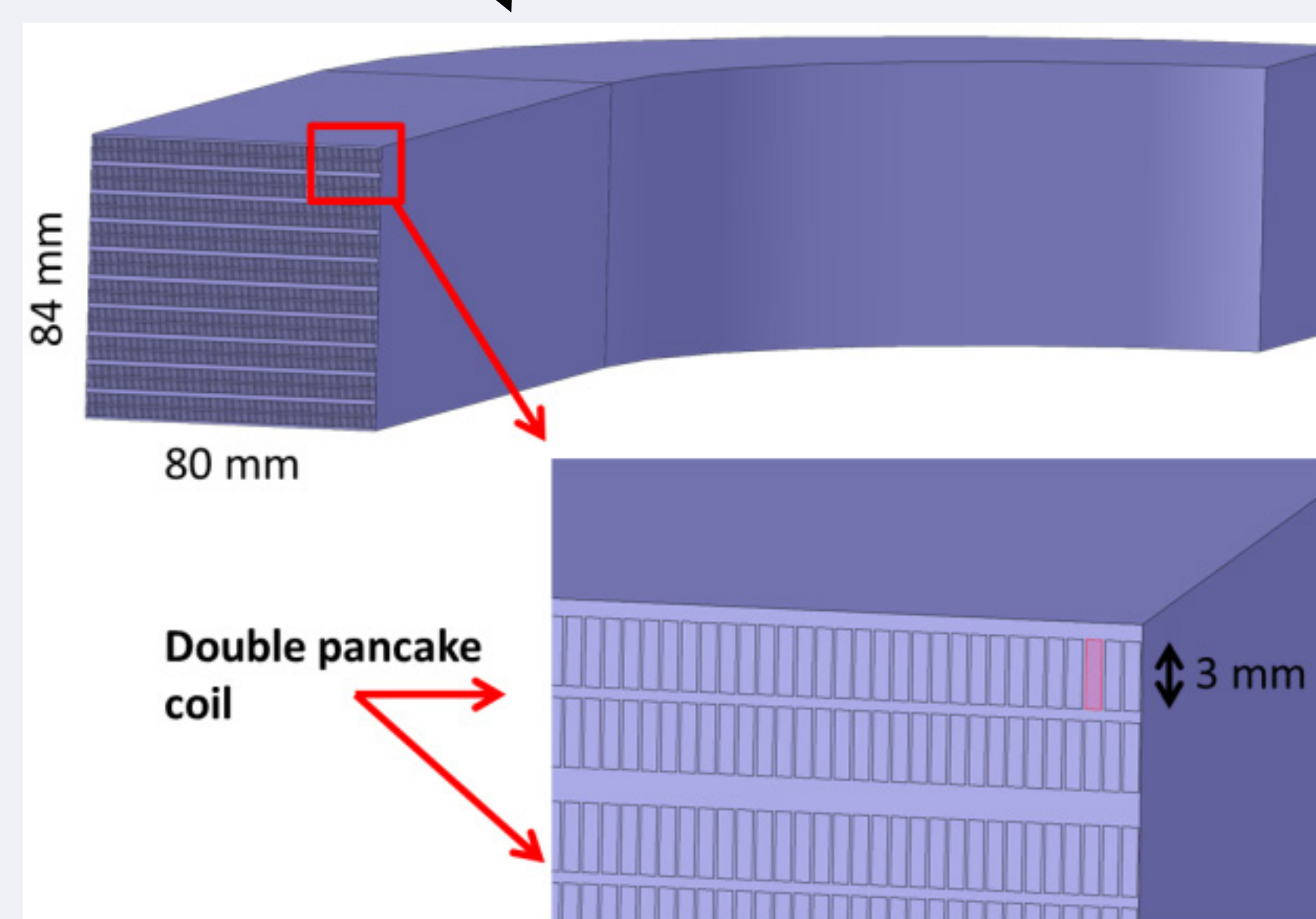
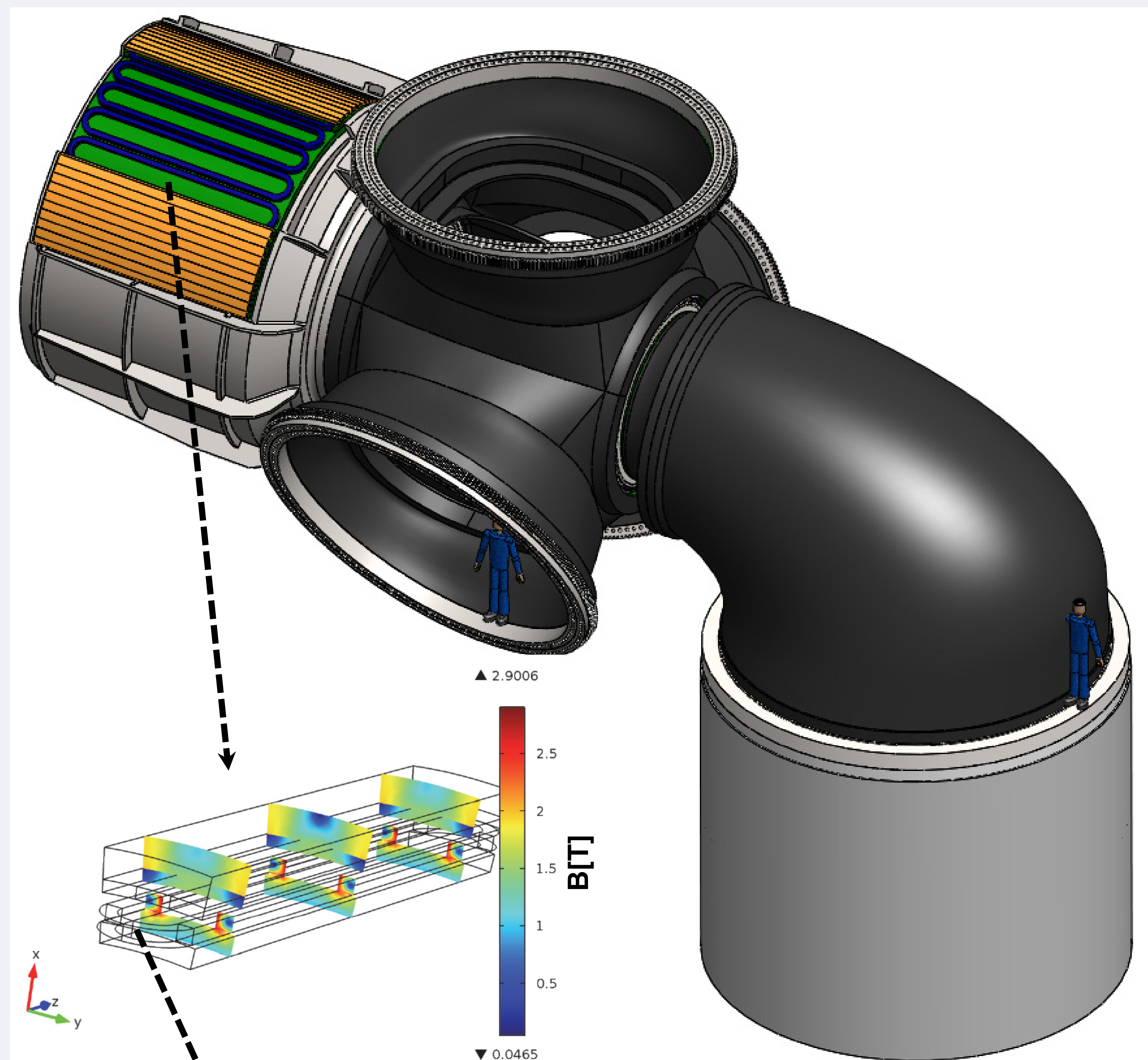
### Generator

- Superconducting field coils and conventional armature winding of Cu
- Air-cored armature windings and magnetic steel shielding
- Non-magnetic support of rotor coils
- Static superconducting field coils and rotating armature with slip ring
- Static cryostat and cryogenic cooling system
- Full rated power electronics
- $D = 5.8$  m &  $L = 3.1$  m to match the hub
- 32 poles &  $f = 2.6$  Hz
- $B_g = 1.5$  T,  $A_s = 100$  kA/m &  $F_d = 75$  kN/m<sup>2</sup>

### Rotor field coils

- MgB<sub>2</sub> superconducting tape ( 3.0 mm x 0.7 mm ) @ 4 ( → 1 ) €/m [2]
- $T_c = 39$  K & minimum bending diameter = 0.15 m
- Race track coil as stack of 10 double pan cake coils (  $D = 0.3$  m )

$R_{Fe\ out}$ [m]	2.94	Torque [MNm]	10.6
$R_{Armature\ out}$ [m]	2.79	Speed [rpm]	9.65
$R_{Armature\ in}$ [m]	2.73	Poles [2p]	32
$R_{Supercond\ out}$ [m]	2.69	Frequency [Hz]	2.57
$R_{Supercond\ in}$ [m]	2.59	$B_{air\ gap}$ [T]	1.5
$L_{generator}$ [m]	3.1	Arm. loading [A/m]	$10^5$
$R_{End}$ [m]	0.15	Arm. Fill [%]	50
$W_{coil}$ [mm]	84	Shear stress [kN/m <sup>2</sup> ]	75
$H_{coil}$ [mm]	80	Efficiency [%] <sup>1</sup>	97.7
$L_{SC\ single\ pancake}$ [m]	740.9	$J_{coil}$ [A/mm <sup>2</sup> ]	70 @ 3 Tesla
$L_{SC\ double\ pancake}$ [m]	1481.7	$J_{tape}$ [A/mm <sup>2</sup> ]	113 @ 3 Tesla
$L_{SC\ Race\ track\ coil}$ [km]	14.82	$M_{Cu}$ [kg]	19415
$L_{SC\ total}$ [km]	474.2	$M_{Fe}$ [kg]	24998
Tape unit cost [€/m]	4 ( → 1 )	$M_{active}$ [kg]	52331
SC cost [k€]	1897 ( → 474 )	Cost Cu [€]	291234
$M_{Superconductor}$ [kg]	7918.1	Cost Fe [€]	74994
$M_{cryostat+cooler}$ [kg]	TBD	Cost total [k€]	2263 ( → 840 )
Cost cryostat	TBD	Cost / cap. [€/kW]	226 ( → 84 )



### Discussion

- Load line of field coil:  $J_E = 70$  A/mm<sup>2</sup> in 2.9 T →  $T_{operation} \sim 10-15$  K [3]
- Cost of active material (SC, Cu & Fe) ~ 226 €/kW ( → 84 €/kW )
- < 300 €/kW threshold: 20 % for drive train of 1.5 M€/MW of turbine cost

## Conclusions

A 10 MW superconducting direct drive wind turbine generator based on MgB<sub>2</sub> wire has been analyzed in terms of properties, amount of wire needed and expected cost of the active materials. The diameter is 5.8 m and the active length is 3.1 m. A king-pin nacelle concept with the superconducting generator mounted in front of the rotor blades has been proposed, because it is believed to be one of the only ways to support a rotor approaching 250 m for a 20 MW turbine. Finally a cost of capacity analysis of the generator shows that the contribution from the active materials is 226 €/kW, which is lower than the INNWIND threshold of 300 €/kW. Cost reductions imposed by a decreasing wire price indicate that the expenses of the cryogenic cooling systems can be accommodated. This will be further investigated in the INNWIND project and compared with conventional drive trains.

## References

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